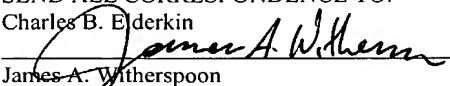
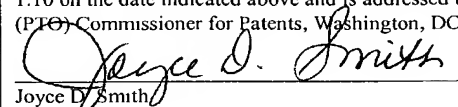


JC20 Rec'd PCT/PTO 29 MAR 2002

FORM PTO-1390 (REV 10-2000)		U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE		ATTORNEY'S DOCKET NUMBER 34691/243030	
TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371				U.S. APPLICATION NO (If known, see 37 C.F.R. 1.5) 10/089635	
INTERNATIONAL APPLICATION NO PCT/DE00/00913		INTERNATIONAL FILING DATE March 24, 2000		PRIORITY DATE CLAIMED September 29, 1999	
TITLE OF INVENTION PRODUCTION OF A DIELECTRIC MULTI-LAYERED REFLECTING COATING					
APPLICANT(S) FOR DO/EO/US Jörg Arnold					
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information					
1. <input checked="" type="checkbox"/> This is a FIRST submission of items concerning a filing under 35 U.S.C. 371					
2. <input type="checkbox"/> This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371					
3. <input checked="" type="checkbox"/> This is an express request to promptly begin national examination procedures (35 U.S.C. 371(f))					
4. <input type="checkbox"/> The US has been elected by the expiration of 19 months from the priority date (PCT Article 31).					
5. <input checked="" type="checkbox"/> A copy of the International Application as filed (35 U.S.C. 371(c)(2)) <ul style="list-style-type: none"> a. <input type="checkbox"/> is attached hereto (required only if not communicated by the International Bureau) b. <input checked="" type="checkbox"/> has been communicated by the International Bureau c. <input type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US) 					
6. <input checked="" type="checkbox"/> A English language translation of the International Application as filed (35 U.S.C. 371(c)(2)).					
7. <input type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)) <ul style="list-style-type: none"> a. <input type="checkbox"/> are attached hereto (required only if not communicated by the International Bureau) b. <input type="checkbox"/> have been communicated by the International Bureau c. <input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired d. <input type="checkbox"/> have not been made and will not be made. 					
8. <input type="checkbox"/> An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3))					
9. <input type="checkbox"/> An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).					
10. <input type="checkbox"/> An English language translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5))					
Items 11. To 16. Below concern other document(s) or information included:					
11. <input type="checkbox"/> An Information Disclosure Statement under 37 C.F.R. 1.97 and 1.98.					
12. <input type="checkbox"/> An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included					
13. <input checked="" type="checkbox"/> A FIRST preliminary amendment. <input type="checkbox"/> A SECOND or SUBSEQUENT preliminary amendment.					
14. <input type="checkbox"/> A substitute specification.					
15. <input type="checkbox"/> A change of power of attorney and/or address letter.					
16. <input type="checkbox"/> Other items or information:					

JC10 Rec'd PCT/PTO 29 MAR 2002

U.S. APPLICATION NO. (If known, see 37 CFR 1.50) 10/089635		INTERNATIONAL APPLICATION NO PCT/DE00/00913		ATTORNEY'S DOCKET NUMBER 34691/243030	
17. <input checked="" type="checkbox"/> The following fees are submitted				CALCULATIONS	PTO USE ONLY
Basic National Fee (37 CFR 1.492(a)(1)-(5)): Neither international preliminary examination fee (37 CFR 1.482) nor International search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO				\$1,040.00	
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO				\$ 890.00	
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search (37 CFR 1.445(a)(2)) paid to USPTO				\$ 740.00	
International preliminary examination fee (37 CFR 1.482) paid to USPTO But all claims did not satisfy provisions of PCT Article 33(1)-(4)				\$ 710.00	
International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4)				\$ 100.00	
ENTER APPROPRIATE BASIC FEE AMOUNT =				\$ 890.00	
Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)).				\$	
CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE		
Total Claims	2 -20 =	0	X \$18.00	\$ 0.00	
Independent Claims	1 - 3 =	0	X \$84.00	\$ 0.00	
MULTIPLE DEPENDENT CLAIM(S) (if applicable)				+ \$280.00	\$
TOTAL OF ABOVE CALCULATIONS =				\$ 890.00	
<input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by one-half.				\$	
SUBTOTAL =				\$ 890.00	
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				\$	
TOTAL NATIONAL FEE =				\$ 890.00	
Fee for recording the enclosed assignment (37 CFR 1.21(h)) The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31) \$40.00 per property +				\$	
TOTAL FEES ENCLOSED =				\$ 890.00	
				Amount to be Refunded	\$
				Charged	\$
a. <input checked="" type="checkbox"/> A check in the amount of \$ 890.00 to cover the above fees is enclosed. b. <input type="checkbox"/> Please charge my Deposit Account No. 16-0605 in the amount of \$ to cover the above fees. A duplicate copy of this sheet is enclosed c. <input checked="" type="checkbox"/> The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 16-0605.					
Note: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.					
SEND ALL CORRESPONDENCE TO: Charles B. Elderkin  James A. Witherspoon REGISTRATION NUMBER 36,723 ALSTON & BIRD LLP Bank of America Plaza 101 South Tryon Street, Suite 4000 Charlotte, NC 28280-4000 Tel Charlotte Office (704) 444-1000 Fax Charlotte Office (704) 444-1111 Customer Number 00826			"Express Mail" Mailing Label Number EL 910632050 US Date of Deposit March 29, 2002 I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to BOX PCT, Attn: DO/US (PTO) Commissioner for Patents, Washington, DC 20231.  Joyce D. Smith		

10,089635

IN THE UNITED STATES DESIGNATED OFFICE (DO/US)

In re: Arnold Attn: DO/US
International Appl. No.: PCT/DE00/00913
International Filing Date: March 24, 2000
For: PRODUCTION OF A DIELECTRIC MULTI-LAYERED REFLECTING
COATING

JC10 Rec'd PCT/PTO 29 MAR 2002

March 29, 2002

Box PCT
Commissioner for Patents
Washington, DC 20231

PRELIMINARY AMENDMENT

Sir:

Kindly amend the above identified application as follows:

In The Claims:

Cancel Claims 3-24, without prejudice.

REMARKS

The present Amendment is submitted for the purpose of deleting the claims which are multiple dependent. It is requested that the Amendment be entered prior to the calculation of the filing fee.

The applicant expressly reserves the right to file a new set of claims which re-instates the subject matter of the cancelled claims.

Respectfully submitted,



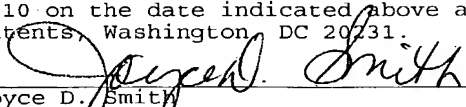
James A. Witherspoon
Registration No. 36,723

ALSTON & BIRD LLP
Bank of America Plaza
101 South Tryon Street, Suite 4000
Charlotte, NC 28280-4000
Tel Charlotte Office (704) 444-1000
Fax Charlotte Office (704) 444-1111
Customer No. 00826
#4527129v1

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Joyce D. Smith

10089635 10/089635

PCT Rec'd 09 JUL 2002

Attorney Docket No. 34691/243030

IN THE UNITED STATES DESIGNATED OFFICE (DO/US)

In re: Arnold Attn: DO/US
International Appl. No.: PCT/DE00/00913
International Filing Date: March 24, 2000
Appl. No. 10/089,635 Conf. No. 3081
For: PRODUCTION OF A DIELECTRIC MULTI-LAYERED
REFLECTING COATING

July 9, 2002

Box PCT
Commissioner for Patents
Washington, DC 20231

SECOND PRELIMINARY AMENDMENT

Sir:

Please amend the above-identified application as follows:

In the Specification:

On page 1, between the title and line 1, insert
--Background of the Invention--.

On page 2, between lines 31 and 32, insert
--Summary of the Invention--.

Please replace the paragraph beginning at page 2, line
32, with the following rewritten paragraph:

--In accordance with the invention, the foregoing object
is accomplished by a method of producing a dielectric
multilayer mirror coating wherein at least two dielectric
layers are initially produced, with each layer having a
predetermined initial thickness. Subsequently, the layers are
arranged, one above the other, to form a stack. Finally, the
thickness of the layered stack and thus the thicknesses of the
individual layers are reduced by deforming the layered stack
while maintaining the thickness ratio or ratios of the layers
relative to one another.--

Please replace the paragraph beginning at page 5, line
13, with the following rewritten paragraph:

In re: Arnold
 Inter'l Appl. No.: PCT/DE00/00913
 Appl. No. 10/089,635
Page 2 of 2

--As regards a high mechanical stability of the mirror coating, the stack of layers may be arranged between two base layers before the deformation and so as to form a "sandwich" block. The layer thickness of the base layers determines the subsequent thickness of the deformed composite material from the layered stack and base layers. The use of thick base layers, which are also deformed at the end of the production process, ensures the necessary tolerance of the individual layer thicknesses after the deformation process, since the attainable layer thickness tolerance of the deformation process is to be related to the thickness of the composite material after the deformation process.--

Please replace the paragraph beginning at page 11, line 6, with the following rewritten paragraph:

--The actual multilayer glass stack that defines the reflection characteristic, is put together between two base glass blocks, whose layer thicknesses determine the subsequent thickness of the rolled out flat glass material or lamp tube material, and a "sandwich" block is formed. The use of thick layers, which are subsequently rolled out, ensures the necessary tolerance of the optical individual thicknesses after rolling, since the attainable layer thickness tolerance of the rolling process is to be related to the total thickness of the flat glass after rolling.--

In the Claims:

Cancel Claims 1 and 2, without prejudice.

Add the following new Claims 25-41:

25. (New) A method of producing a dielectric multilayer mirror coating comprising the steps of
 producing at least two dielectric layers of predetermined

In re: Arnold
Inter'l Appl. No.: PCT/DE00/00913
Appl. No. 10/089,635
Page 3 of 3

initial thicknesses,

arranging the layers one above the other to form a stack of layers,

arranging the stack of layers between two base layers to form a sandwich block,

reducing the thickness of the sandwich block by deforming the sandwich block while maintaining the thickness ratio or thickness ratios of the dielectric layers relative to one another,

wherein the deforming step comprises a series of partial deformation steps, and

wherein at least one of the base layers is formed of a plurality of individual layers which are sequentially built up between the partial deformation steps.

26. (New) The method of Claim 25 wherein the initial thickness of the at least two dielectric layers are different.

27. (New) The method of Claim 25 wherein at least one dielectric layer of the stack comprises glass or plastic.

28. (New) The method of Claim 25 wherein the at least two dielectric layers have different indices of refraction.

29. (New) The method of Claim 25 wherein the at least two dielectric layers form a double layer.

30. (New) The method of Claim 29 wherein at least two double layers are stacked.

31. (New) The method of Claim 30 wherein the thickness varies from double layer to double layer.

32. (New) The method of Claim 25 wherein the step of arranging the layers one above the other includes a stacking and/or roll-up of the layers.

41. (New) The method of Claim 25 wherein the individual layers of the at least one of the base layers are fused together during the partial deformation steps.

In re: Arnold
Inter'l Appl. No.: PCT/DE00/00913
Appl. No. 10/089,635
Page 5 of 5

REMARKS

The present Amendment is for the purpose of presenting the specification and claims in a more acceptable format under U.S. practice.

An early and favorable consideration is solicited.

Respectfully submitted,



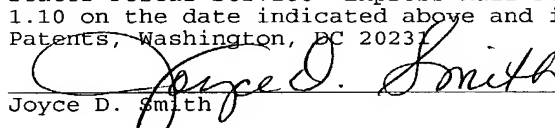
Charles B. Elderkin
Registration No. 24,357

ALSTON & BIRD LLP
Bank of America Plaza
101 South Tryon Street, Suite 4000
Charlotte, NC 28280-4000
Tel Charlotte Office (704) 444-1000
Fax Charlotte Office (704) 444-1111
Customer No. 00826
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Joyce D. Smith

In re: Arnold
Inter'l Appl. No.: PCT/DE00/00913
Appl. No. 10/089,635
Page 6 of 6

Version With Markings to Show Changes Made

In the Specification:

The paragraph beginning at page 2, line 32, has been amended as follows:

In accordance with the invention, the foregoing object is accomplished by a method of producing a dielectric multilayer mirror coating wherein [by the characterizing steps of claim 1. Accordingly,] at least two dielectric layers are initially produced, with each layer having a predetermined initial thickness. Subsequently, the layers are arranged, one above the other, to form a stack. Finally, the thickness of the layered stack and thus the thicknesses of the individual layers are reduced by deforming the layered stack while maintaining the thickness ratio or ratios of the layers relative to one another.

The paragraph beginning at page 5, line 13, has been amended as follows:

As regards a high mechanical stability of the mirror coating, [it would be possible to arrange] the stack of layers may be arranged between two base layers before the deformation and so as to form a "sandwich" block. The layer thickness of the base layers determines the subsequent thickness of the deformed composite material from the layered stack and base layers[, and a "sandwich" material results]. The use of thick base layers, which are also deformed at the end of the production process, ensures the necessary tolerance of the individual layer thicknesses after the deformation process, since the attainable layer thickness tolerance of the deformation process is to be related to the thickness of the composite material after the deformation process.

The paragraph beginning at page 11, line 6, has been

In re: Arnold
 Inter'l Appl. No.: PCT/DE00/00913
 Appl. No. 10/089,635
Page 7 of 7

amended as follows:

The actual multilayer glass stack that defines the reflection characteristic, is put together between two base glass blocks, whose layer thicknesses determine the subsequent thickness of the rolled out flat glass material or lamp tube material, and a [. A] "sandwich" block [material] is formed. The use of thick layers, which are subsequently rolled out, ensures the necessary tolerance of the optical individual thicknesses after rolling, since the attainable layer thickness tolerance of the rolling process is to be related to the total thickness of the flat glass after rolling.

#4529880v1

PROCESS FOR PRODUCTION OF A DIELECTRIC MULTI-LAYERED
REFLECTING COATING

The invention relates to a method of producing a dielectric multilayer mirror coating.

Dielectric multilayer mirror coatings, i.e., mirror coatings consisting of a plurality of dielectric layers have been used for a long time for a spectrally selective conveyance of reflection or transmission in the case of optical windows and other optical components and devices. Furthermore, it is known to apply a mirror coating to bulbs of lamps. The object of such mirror coatings always consists in reflecting certain portions of radiation, whereas certain other portions of radiation are transmitted with certain other wavelengths.

In a conventional method, such multilayer mirror coatings are produced by applying individual dielectric layers, which are generally composed of two different dielectric materials and have, if possible, different indices of refraction. In general, the layers are applied by vacuum evaporation or by precipitation from a solution. The mirror coating is then produced in that a double layer consisting of, for example, two different materials is layered several times, so as to result in a periodic sequence of the different layers.

The different layers must have a layer thickness that is to be kept exactly within narrowest tolerances for purposes of achieving the required mirror quality and spectral reflection- and transmission characteristic. Normally, optical layer thickness means the geometric layer thickness, which is multiplied by the refractive index of the dielectric material of the layer. The optical thickness may vary from double layer to double layer in a predetermined manner.

The conventional production process of such dielectric multilayer mirror coatings is complicated. For example, costly and expensive high-vacuum evaporation plants are used. In this process, it is necessary to
5 apply the layers individually, one after the other. Furthermore, the mirror coating process can be performed only within the scope of a batch production. A mass production within the scope of an assembly line production is not possible in the case of the closed
10 high-vacuum evaporation technique. Furthermore, the mirror quality that can be obtained by applying the layers individually one after the other is limited. In a conventional manner, it is possible to apply to curved surfaces on a commercial scale only at most as many as 70
15 dielectric layers or 35 dielectric double layers. With that, it is possible to obtain for a broadband mirror coating a reflection coefficient of 0.7. In the conventional method, an all around extending dielectric multilayer mirror coating of, for example, cylindrical
20 objects is technologically not possible. With that, it is possible to apply dielectric multilayer mirror coatings by evaporation only to flat or little curved surfaces such as, for example, lens surfaces.

In summary, it is possible to achieve with known
25 multilayer mirror coatings, a reflection coefficient of at most 0.7.

It is therefore an object of the present invention to describe a method of producing a dielectric multilayer mirror coating, which permits realizing in a simple
30 manner a multilayer mirror coating with an increased coefficient of reflection.

In accordance with the invention, the foregoing object is accomplished by a method of producing a dielectric multilayer mirror coating by the

characterizing steps of claim 1. Accordingly, at least two dielectric layers are initially produced, with each layer having a predetermined initial thickness.

Subsequently, the layers are arranged, one above the other, to form a stack. Finally, the thickness of the layered stack and thus the thicknesses of the individual layers are reduced by deforming the layered stack while maintaining the thickness ratio or ratios of the layers relative to one another.

In a way according to the invention, it has been recognized that besides the known methods of producing a dielectric multilayer mirror coating -- vapor depositing individual layers or precipitating layers from a solution -- there also exists a further possibility of producing dielectric multilayer mirror coatings, wherein lastly the desired number of layers is initially arranged one above the other to form a layered stack. In so doing, it is essential that the thicknesses of the layers be selected such that the thickness ratios of the layers relative to one another are correct. The individual layers may be much thicker than in the final state of the mirror coating, which simplifies handling of the individual layers considerably. In the further process, the thickness of the layered stack or the thicknesses of the individual layers are considerably reduced, if need be, by a deformation step. However, the thickness ratios of the layers relative to one another remain unchanged. In other words, the layered stack is predetermined "macroscopically," so as to be present "microscopically" upon completion of the production process.

In the production method of the present invention, a technical limitation of the maximum number of layers to the range of 70 individual layers or 35 double layers is nonexistent. Consequently, it is possible to reflect in

a predetermined wavelength interval, the wavelengths of which are, for example, to be reflected, a substantially larger number of wavelengths, to which individual layers or double layers are respectively associated for reflection. In this connection, it is quite realistic to use, for example, 400 double layers. This results in a considerably higher reflection coefficient than the reflection coefficient of 0.7 that has so far been reachable.

Consequently, the method of the present invention for producing a dielectric multilayer mirror coating defines a method, which permits realizing in a simple manner a multilayer mirror coating with an increased coefficient of reflection.

Within the scope of producing the dielectric layers, the initial thicknesses of the layers are predetermined. In this connection, the initial thicknesses of at least two layers could be different. When more than two layers are provided, all layers could be differently thick, or even groups of layers could have the same thickness. Any combination is possible, with the thicknesses having to be adapted to the wavelengths of the radiation that is to be reflected.

In a particularly simple manner, it would be possible to make at least one layer from glass or plastic. In this connection, combinations of glass and plastic or even uniform layered stacks of glass and plastic are possible.

For an effective reflection of the desired radiation, at least two layers could have different indices of refraction. However, it would also be possible that all layers have different indices of refraction.

Furthermore, a double layer could be produced from two layers. In a further development, it would be possible to stack at least two double layers, with the optical layer thickness varying from double layer to double layer.

Concretely, the arrangement of the layers, one above the other, could be a stacking of the layers. As an alternative thereto, the arrangement could also comprise a roll-up of the layers. In this instance, two layers are initially stacked one above the other, and then rolled up as one. With that, it would be possible to obtain a regular sequence of the one and the other layer.

As regards a high mechanical stability of the mirror coating, it would be possible to arrange the stack of layers between two base layers before the deformation. The layer thickness of the base layers determines the subsequent thickness of the deformed composite material from the layered stack and base layers, and a "sandwich" material results. The use of thick base layers, which are also deformed at the end of the production process, ensures the necessary tolerance of the individual layer thicknesses after the deformation process, since the attainable layer thickness tolerance of the deformation process is to be related to the thickness of the composite material after the deformation process.

As regards a simple handling of the base layers, at least one base layer could be formed from a plurality of individual layers. Such individual layers could be arranged on a preceding layer, preferably melted thereto step by step, each time subsequent to a partial deformation process.

In a simple manner, the base layers or individual layers could be formed from glass. With that, it would

also be possible to have a base layer in the form of base glass block.

For a reliable optical connection of the layers, it would be possible to join the layers by fusing them together after arranging them one above the other. To prevent air bubbles from forming between the individual layers, the fusion could occur under vacuum. However, the bonding temperature should be reached and maintained only a short time, for purposes of avoiding a diffusion or a convective transportation of the different layer constituents into the adjoining different layers and, thus, a blurring of the difference in the refractive index of the different layers.

As regards the deformation of the layered stack and, if need be, of the base layers, different methods are possible. On the one hand, deformation could occur by pressing. As an alternative thereto, deformation could occur by rolling, wherein likewise a kind of pressing is, applied. In a further alternative, deformation could occur by a drawing operation of the layered stack. All methods permit reducing the layer thicknesses to the necessary, very small layer thicknesses, while maintaining the layer thickness ratios.

A simplified deformation could occur by the action of heat. However, in this instance, one should observe that the applied temperatures be not too much above the temperature of the mechanical yield point of the layer materials, so that no unwanted material transportation by, for example, diffusion or convection, leads to a penetration or intermixing of the different layer materials, thereby removing or deforming unintentionally the geometric limits that are to be maintained.

For a most extensive prevention of any diffusion- or convection processes, the deformation could occur without supplying additional heat.

As regards an economically interesting application,
 5 it would be possible to produce from the deformed stack of layers, tubes or curved panes. Tubes could be used, for example, as a source material for lamp bulbs. Curved panes could be used in the manufacture of automobiles.

In the presence of base layers it will be
 10 advantageous, when the layered stack or the actual dielectric multilayer is located very close below one of the surfaces of the composite material, namely in the vicinity of an inner surface of the tubes or curved panes. With that, it is possible to attain a high
 15 degrees of reflection of, for example, infrared radiation that is produced in the interior, with a residual absorption of the infrared radiation being minimized in the composite material consisting of base layers and the layered stack.

20 On the one hand, the multilayer mirror coating may be realized within the scope of a multilayer mirror. In this instance, the layered stack is quasi self-supporting without any further base layers.

As an alternative thereto, the multilayer mirror
 25 coating could be realized within the scope of a multilayer mirror coating on a base body. In this instance, the layered stack is arranged on an essentially supporting base body or an individual base layer.

A third alternative, namely the possibility of
 30 arranging the layered stack between two base layers has already been described further above. In this instance a base structure is provided on both sides of the layered stack.

The method of present invention permits producing mirror coatings, which may be subjected to a further uniform deformation -- for example, the production of cylindrical tubes or curved window panes -- without interfering with the mirror characteristics or the dielectric layer ratios. Thus, it is possible to produce, for example, dielectric multilayer jackets for, for example, cylindrical lamp bodies or lamp bulbs. This again permits separating the mirror coating of, for example, lamps, as a production step from the lamp production itself. Furthermore, it is possible to produce flat glass panes, automobile glass panes, automobile headlight panes or lamp bulbs, which already bring along the required mirror coating properties in a material-inherent fashion, so as to omit the mirror coating process of such objects as a separate production step. The mirror coating properties are determined by the arrangement of the layers of quasi any desired thickness and quasi any desired periodic sequences.

Extensive tests were conducted with respect to the glass technological use of a dielectric multilayer glass material. The production process of a dielectric multilayer material is advantageously divided into three production steps. In a first production step, a multilayer glass stack is produced. In a second production step, this stack is rolled out to a flat glass, and in a third production step, tubes for the lamp production or production of lamp bulbs are manufactured from the flat glass material.

In the modern lamp technology, it will be advantageous, when the lamp bulb reflects a large portion of the heat radiation emitted by a filament or glow wire again back to the filament or glow wire. This enables a backheating of the filament or glow wire, whereby it is

made possible to supply for reaching the same filament-
or glow wire temperature, less electrical energy to the
filament or glow wire than in conventional lamps without
reflecting bulbs. The more heat radiation can be
5 reflected from the inner side of the lamp bulb, the more
favorable the conversion efficiency between supplied
electrical power and radiated and transmitted visible
light of the filament or glow wire. Consequently, in the
case of modern lamps, a high coefficient of reflection
10 for heat radiation, i.e. for radiation in a certain
wavelength interval is desired. The multilayer mirror
coating produced in accordance with the invention allows
to achieve a very high coefficient of reflection in the
desired wavelength interval.

15 To this end, multilayer glass stacks are prepared in
accordance with the required optical reflection- or
transmission characteristic. The spectral transmission
range should be, for example between the wavelengths λ_0
and λ_1 . The spectral range of reflection should be, for
20 example, between the wavelengths γ_1 and γ_2 . For a
broadband reflection with a high coefficient of
reflection between the wavelengths λ_1 and λ_2 , the
individual layer thicknesses d_i are increased continuously
or stepwise between the layer thickness limits $d_1 =$
25 $k\lambda_1/(4n_{11})$ and $d_2 = k\lambda_2/(4n_{21})$ with the respective
refraction indices n_i of the two different types of glass
in use. In this instance, the $\lambda/4$ condition of the
optical path applies, where k is the dilatation factor of
the glass stack thickness during the entire rolling
30 process.

However, for the layer thickness limit d_2 and, thus,
for the band width of the reflection, the marginal
condition is that $d_2 < k \cdot 3\lambda_0/(4n_{01})$, because otherwise the
light of the limit wavelength γ_0 , which is to be maximally

transmitted is likewise maximally reflected. For a refractive index averaging $n_0 = 1.59$ with the short-wave transmission limit $\lambda_0 = 0.4 \mu\text{m}$, the long-wave reflection limit with a there assumed mean refractive index of $n_2 =$
5 1.53 is $\lambda_2 = 3 \lambda_0 n_2/n_0 = 1.15 \mu\text{m}$.

However, this applies only to portions of radiation with a vertical incidence on the mirror coating. For portions of radiation, which strike the mirror coating at a different angle of incidence, the short-wave reflection
10 limit shifts toward shorter wavelengths, and the long-wave reflection limit toward longer wavelengths. For this reason, it is possible to attain in the case of a required transmission range from 400 nm to 700 nm in total, reflection ranges from about 700 nm to about 2μ
15 with a high reflectivity.

The here proposed production method allows to use a very large number of dielectric layers, which may amount to more than 50, and typically to several hundred dielectric layers. As a result, it is possible to use a
20 small difference in the refractive index of low refracting glass types, because the larger possible number N of dielectric double layers compensates the small differences in the index of refraction, so that one can expect a high coefficient of reflection $R_{2N+1} = (1 -$
25 $n_1/n_2^{2N})^2 / (1 + n_1/n_2^{2N})^2$. For example, for 400 double layers in 10 stepped stacks with the two mean indices of refraction in the spectral reflection range of 1.5 for crown glass and 1.6 for heavy crown glass relative to air with the refractive index of 1, it is possible to
30 estimate a maximum coefficient of reflection of 0.98.

For fusing together the multilayer glass stack, a vacuum melting process is used to prevent air bubbles from forming between the glass layers. The bonding temperature should be reached and held only for a short

time for purposes of suppressing a diffusion or a convective transportation of the different glass constituents into adjoining, different glass layers and, thus, a blurring of the difference in the refractive index of the different glass layers.

The actual multilayer glass stack that defines the reflection characteristic, is put together between two base glass blocks, whose layer thicknesses determine the subsequent thickness of the rolled out flat glass material or lamp tube material. A "sandwich" material is formed. The use of thick layers, which are subsequently rolled out, ensures the necessary tolerance of the optical individual thicknesses after rolling, since the attainable layer thickness tolerance of the rolling process is to be related to the total thickness of the flat glass after rolling.

The tolerance Δd_i of an optical $\lambda/4$ layer is $\Delta d_i = \Delta d/k$. The attainable tolerance Δd of the flat glass production amounts in absolute terms to as much as 3/100 mm for, for example, microscopic cover glasses. For a sandwich block with 400 dielectric double layers averaging two times the microscopic cover glass thickness -- namely, 3/10 mm double layer thickness before rolling -- and a required double layer thickness averaging twice the $\lambda/4$ thickness $2d_i = 0.33 \mu\text{m}$ -- with a wavelength of 1 μm and a corresponding average glass refraction index of 1.5 after rolling, and having a required flat glass thickness of 1 mm after rolling, the tolerance to be maintained is about 30 nm per optical layer.

The multilayer stack is arranged between a base glass cover and a base glass bottom. On the one hand, it is the object of the base glass cover and base glass bottom to determine the subsequent flat glass thickness, and on the other hand, it is their object to prevent

superficial layer distortions during the rolling process, so that the dielectric multilayer region in-between remains unaffected by the edge distortions of the rolling process. The entire sandwich block has a layer thickness $D = d/k$, where k is the dilatation factor, and d the desired flat glass thickness after the rolling process.

As an example, the dimensions of a sandwich block with 400 dielectric double layers, which is to be rolled out to a 1 mm thick flat glass, are listed before and after rolling.

Sandwich block dimensions	Before rolling	After rolling
Individual layer thickness	$0.15 \times 10^{-3} \text{ m}$	$0.167 \times 10^{-6} \text{ m}$
Thickness of 400 double layers	0.12 m	$0.1336 \times 10^{-3} \text{ m}$
Base layer thickness	0.78 m	$0.8664 \times 10^{-3} \text{ m}$
Sandwich thickness	0.9 m	$1 \times 10^{-3} \text{ m}$
Absolute tolerance per layer thickness	$0.03 \times 10^{-3} \text{ m}$	$33.3 \times 10^{-9} \text{ m}$
Dilatation factor	1/900	1/900

To be still able to handle in the rolling process the large initial layer thickness of the sandwich block of 90 cm as shown in the example, it is possible to replace the base glass blocks with a plurality of glass plates of the same total thickness, which are then fused together with the sandwich step by step subsequent to a respective partial rolling process.

The further processing of the mirror glass material for the lamp production can be carried out by the existing flat glass production technology. At the end of the production process, the resultant rolled glass can be rolled and manufactured to glass tubes for a lamp production. In this connection, the actual dielectric multilayer, which is located, for example, very close

coatings, which have so far not been possible from the viewpoint of shaping.

As regards further advantageous improvements and further developments of the teaching according to the invention, the attached claims are herewith incorporated
5 by reference.

Finally, it should be expressly emphasized that the foregoing, merely arbitrarily selected example with, for example, 400 double layers, is used only for explaining
10 the invention, without however limiting same to this example.

C L A I M S

1. Method of producing a dielectric multilayer mirror coating,

5 **characterized by** the following steps:

- producing at least two dielectric layers of predetermined initial thicknesses;

- arranging the layers one above the other for forming a stack of layers; and

10 - reducing the thickness of the layered stack and thus the thickness of the individual layers by deforming the layered stack while maintaining the thickness ratio or thickness ratios of the layers relative to one another.

15

2. Method of claim 1, characterized in that the initial thicknesses of the at least two layers are different.

20

3. Method of claim 1 or 2, characterized in that at least one layer is made of glass.

4. Method of one of claims 1-3, characterized in that at least one layer is made of plastic.

25

5. Method of one of claims 1-4, characterized in that at least two layers have different indices of refraction.

30

6. Method of one of claims 1-6, characterized in that a double layer is produced from two layers.

7. Method of claim 6, characterized in that at least two double layers are stacked.

8. Method of claim 7, characterized in that the optical layer thickness varies from double layer to double layer.

5

9. Method of one of claims 1-8, characterized in that the arranging process includes a stacking and/or roll-up of the layers.

10

10. Method of one of claims 1-9, characterized in that the layered stack is arranged between two base layers before the deformation.

15

11. Method of claim 10, characterized in that at least one base layer is formed from a plurality of individual layers.

20

12. Method of claim 11, characterized in that the individual layers are arranged on a preceding layer, preferably melted thereto, step by step each time subsequent to a partial deformation process.

25

13. Method of one of claims 10-12, characterized in that the base layers or individual layers are formed from glass.

30

14. Method of one of claims 1-13, characterized in that the layers are joined by fusion after arranging the layers one above the other.

15. Method of claim 14, characterized in that the melting occurs under vacuum.

17. Method of one of claims 1-16, characterized in
5 that the deformation occurs by a rolling operation.

10 19. Method of one of claims 1-18, characterized in
that the deformation occurs by the action of heat.

20. Method of one of claims 1-18, characterized in
that the deformation occurs without a supply of
15 additional heat.

21. Method of one of claims 1-20, characterized in that tubes or curved panes are produced from the deformed stack of layers.

22. Method of claim 21, characterized in that the layered stack is arranged in the vicinity of an inner surface of the tubes or curved panes.

25 23. Method of one of claims 1-22, characterized in
that the multilayer mirror coating is realized within the
scope of a multilayer mirror.

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ABSTRACT

A method of producing a dielectric multilayer mirror coating is characterized with a view to increasing the coefficient of reflection by the following steps: to begin with, at least two dielectric layers of predetermined initial thicknesses are produced. Subsequently, the layers are arranged one above the other for forming a layered stack. Finally, the thickness of the stack of layers and thus the thicknesses of the individual layers are reduced by deforming the layered stack while maintaining the thickness ratio or ratios of the layers relative to one another.

15

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(12) NACH DEM VERTRAG ÜBER DIE INTERNATIONALE ZUSAMMENARBEIT AUF DEM GEBIET DES
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von US): MITSUBISHI INTERNATIONAL GMBH
[DE/DE]; Kennedydamm 19, D-40476 Düsseldorf (DE).

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(72) Erfinder; und

(75) Erfinder/Anmelder (nur für US): ARNOLD, Jörg
[DE/DE]; Friedrich-Ebert-Anlage 46, D-69117 Heidelberg
(DE).Zur Erklärung der Zweibuchstaben-Codes, und der anderen
Abkürzungen wird auf die Erklärungen ("Guidance Notes on
Codes and Abbreviations") am Anfang jeder regulären Ausgabe
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(54) Title: PROCESS FOR PRODUCTION OF A DIELECTRIC MULTI-LAYERED REFLECTING COATING

(54) Bezeichnung: VERFAHREN ZUR HERSTELLUNG EINER DIELEKTRISCHEN MEHRSCICHTVERSPIEGELUNG

(57) Abstract: A process for the production of a dielectric multi-layered reflecting coating with a view to increasing the reflection coefficient is characterised by the following steps: initially, at least two dielectric layers of a given primary thickness are formed; the layers are then arranged on top of each other to form a stack. Finally, the thickness of said stack is reduced by deformation, whereby the thickness ratios or the thickness ratios between each layer are retained.

(57) Zusammenfassung: Ein Verfahren zur Herstellung einer dielektrischen Mehrschichtverspiegelung ist im Hinblick auf eine Erhöhung des Reflexionskoeffizienten durch die folgenden Schritte gekennzeichnet. Zunächst erfolgt ein Bereitstellen von zumindest zwei dielektrischen Schichten vorgegebener anfänglicher Dicken. Dann werden die Schichten zur Bildung eines Schichtpakets übereinander angeordnet. Schliesslich werden die Dicke des Schichtpakets und damit die Dicken der einzelnen Schichten durch ein Verformen des Schichtpakets unter Beibehaltung des Dickenverhältnisses oder der Dickenverhältnisse der Schichten zueinander reduziert.

WO 01/23915 A1

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PRODUCTION OF A DIELECTRIC MULTI-LAYERED REFLECTING COATING

the specification of which is attached hereto unless the following box is checked:

☒ was filed on March 24, 2000
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International Application Number
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Priority Not Claimed
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Charles B. Elderkin
Reg. No. 24,357 and All Attorneys registered with
Customer Number 000826

Postanschrift:

Send Correspondence to:
Customer No. 000826

Telefonische Auskünfte: (Name and Telefonnummer)

Direct Telephone Calls to: (name and telephone number)
Charles B. Elderkin
(704) 444-1000

Vor-und Zuname des einzigen oder ersten Erfinders (2)		Full name of sole or first inventor	
Unterschrift des Erfinders		Inventor's signature	
Datum		Date	
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Postanschrift		Post Office Address	

Jörg Arnold *Dr Jörg Arnold*
Heidelberg, Germany **DEX**
Germany
Friedrich-Ebert-Anlage 46
D-69117 Heidelberg, Germany

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